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Anisotropic Vector Play Model Incorporating Decomposed Shape Functions

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We propose an accurate anisotropic vector play model that uses the decomposition of vector shape functions. The parallel and perpendicular components of the magnetic field H to the magnetic flux density B are independently identified in constructing the decomposed shape functions. We further propose a method to reconstruct the perpendicular component from the one-dimensional measurement of the parallel component based on a magnetic energy approach. This method accurately reconstructs the vector hysteretic properties of silicon steel under alternating and rotating magnetic flux conditions.

Index Terms— Anisotropy, magnetic energy, play model, vector hysteresis.

I. INTRODUCTION

ADVANCED magnetic field analyses of three-phase electric machinery require precise descriptions of the vector hysteretic property of the magnetic field at junctions of magnetic flux. The vector play model [1]–[4] is one of the most accurate and efficient models in representing the vector hysteretic property of silicon steel sheets.

Using the isotropic vector play model and the anisotropy matrix, Ref. [4] describes a successful approximation to the anisotropic vector hysteresis of non-oriented silicon steel sheets including the elliptic rotational field. In representing the dynamic vector hysteretic property, the model provides a base model of the dynamic model [5] or it is applied to the finite element eddy-current analysis [6]. However, because of the simple construction of the anisotropy matrix, the representation may not be highly accurate when the anisotropy becomes strong. Another drawback of this model is the need to measure the alternating magnetic property using a 2D or rotational single sheet tester (SST) [7], where precise waveform control is needed to maintain the B-vector along its specified direction.

For an accurate anisotropy representation, this paper proposes anisotropic shape functions that represent the perpendicular component of the magnetic field H to the magnetic flux density B independently of its parallel component. Based on a magnetic energy approach [8], [9], we further propose a method to reconstruct the perpendicular component without its direct measurement using only the 1-D measurement of the parallel component.

II. VECTOR PLAY MODEL

From the magnetic flux density B as input, the anisotropic vector play model provides the magnetic field H as output:

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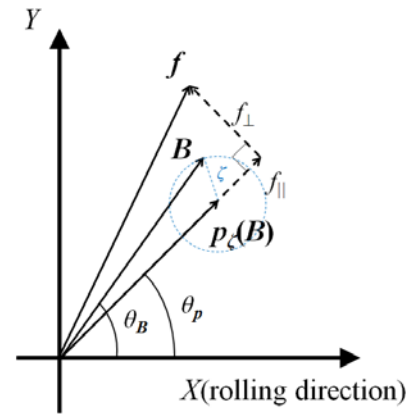


Fig.1. Vector play hysteron and vector shape function.

$$H = P(B) = \int_0^{B_s} f(\zeta, p_\zeta(B), B) d\zeta, \quad (1)$$

$$p_\zeta(B) = B - \frac{\zeta(B - p_\zeta^0)}{\max(\zeta, |B - p_\zeta^0|)}, \quad (2)$$

where f is the anisotropic vector shape function, p_ζ is the vector play hysteron having radius ζ , p_ζ^0 is the vector p_ζ at the previous time-point, and B_s is the saturation magnetic flux density. Ref. [4] proposed a simple form for the shape function,

$$f(\zeta, p_\zeta(B), B) = W(|B|, \theta_B) f_0(\zeta, p_\zeta(B)), \quad (3)$$

where W is the anisotropy matrix, θ_B the azimuth angle of B , and f_0 the isotropic vector shape function.

We propose two more accurate representations of the vector shape function,

$$f(\zeta, p_\zeta(B), B) = f_{\parallel}(\zeta, |p_\zeta(B)|, \theta_B) e_{p_{\parallel}} + f_{\perp}(\zeta, |p_\zeta(B)|, \theta_B) e_{p_{\perp}} \quad (4)$$

and

$$f(\zeta, p_\zeta(B)) = f_{\parallel}(\zeta, |p_\zeta(B)|, \theta_p) e_{p_{\parallel}} + f_{\perp}(\zeta, |p_\zeta(B)|, \theta_p) e_{p_{\perp}} \quad (5)$$

where θ_p is the azimuth angle of p_ζ , f_{\parallel} and f_{\perp} are the shape functions for the parallel and perpendicular component of H to p_ζ , and $e_{p_{\parallel}}$ and $e_{p_{\perp}}$ denote the parallel and perpendicular unit vectors to p_ζ (see Fig. 1). For the anisotropy representation, the shape functions, (4) and (5), depend on the azimuth angles of B and p_ζ , respectively.

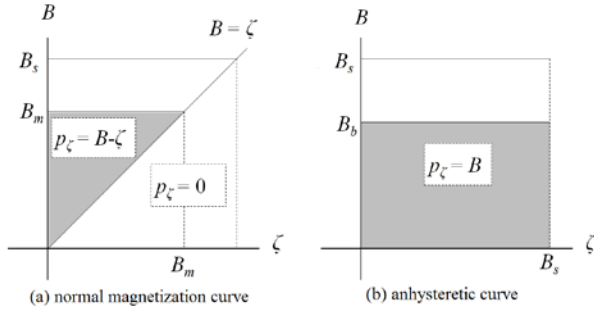


Fig. 2. Integral domains for the normal magnetization and anhysteretic curves

The shape functions $f_{||}$ and f_{\perp} are determined from the measured parallel and perpendicular components of $\mathbf{H} = (H_{||}(B, \theta_B), H_{\perp}(B, \theta_B))$ using the identification method for a scalar play model [10].

III. MAGNETIC ENERGY APPROACH

A. Magnetic energy and 2-D magnetic property

The vector components of $(H_{||}(B, \theta_B), H_{\perp}(B, \theta_B))$ are measured under the alternating flux condition along the θ_B -direction. The measurement of $H_{\perp}(B)$ requires the 2-D SST, where a sophisticated waveform control is required to maintain \mathbf{B} along its specified direction. In contrast, $H_{||}(B, \theta_B)$ can be measured by the conventional 1-D SST or the Epstein frame using strip samples cut along the θ_B directions.

Refs. [8] and [9] proposed a useful method to determine $H_{\perp}(B, \theta_B)$ without its measurement using the magnetic energy. The magnetic energy density F is defined as

$$F(B, \theta_B) = \int_0^B \mathbf{H} \cdot d\mathbf{B} = \int_0^B H_{||}(B, \theta_B) dB. \quad (6)$$

It is assumed that \mathbf{H} and \mathbf{B} have no hysteretic relation and that the integration is independent of the path. Using the magnetic energy (6), the components of \mathbf{H} are given as

$$H_{||} = \frac{\partial F}{\partial B}, \quad H_{\perp} = \frac{1}{B} \frac{\partial F}{\partial \theta_B}. \quad (7)$$

As (7) is derived without hysteresis, it cannot be used directly to determine f_{\perp} but can be obtained with a method developed below via two magnetization curves without hysteresis, the normal magnetization curve and the anhysteretic curve, to be applied in (6) and (7)

B. Derivation from normal magnetization curve

The normal magnetization curve is obtained by the measurement of symmetric B - H loops under the alternating magnetic flux condition. The play model does not distinguish the normal magnetization curve from the initial magnetization curve. For the alternating input of amplitude B_m along the θ_B -direction, the input $\mathbf{B} = B_m \mathbf{e}_{B||}$ gives

$$\mathbf{p}_{\zeta}(B_m \mathbf{e}_{B||}) = \begin{cases} (B_m - \zeta) \mathbf{e}_{B||} & (\zeta < B_m) \\ 0 & (B_m \leq \zeta) \end{cases}, \quad (8)$$

where $\mathbf{e}_{B||}$ is the unit vector parallel to \mathbf{B} . Assuming $f_{||}(\zeta, 0, \theta) = f_{\perp}(\zeta, 0, \theta) = 0$, $\mathbf{H}_m(B_m \mathbf{e}_{B||}) = (H_{m||}, H_{m\perp})$ is given by

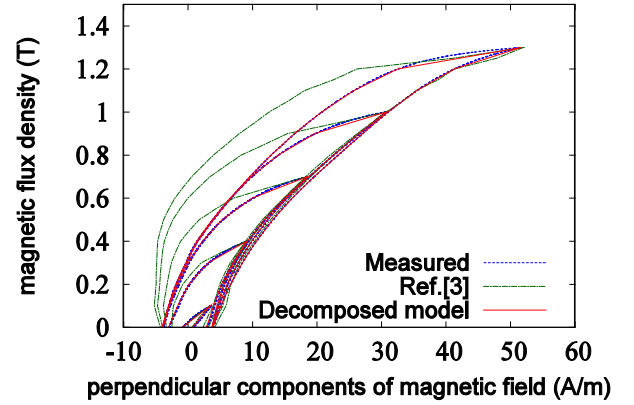


Fig. 3. Simulated B - H_{\perp} loops for $\theta_B = \pi/6$ using the shape functions (3) and (4), where f_{\perp} in (4) is identified from measured data.

$$H_{m||}(B_m, \theta_B) = \int_0^{B_m} f_{||}(\zeta, B_m - \zeta, \theta_B) d\zeta, \quad (9)$$

$$H_{m\perp}(B_m, \theta_B) = \int_0^{B_m} f_{\perp}(\zeta, B_m - \zeta, \theta_B) d\zeta. \quad (10)$$

From (6) and (9), the magnetic energy density F is represented as

$$\begin{aligned} F(B_m, \theta_B) &= \int_0^{B_m} H_{m||}(B, \theta_B) dB \\ &= \int_0^{B_m} \left\{ \int_0^B f_{||}(\zeta, B - \zeta, \theta_B) d\zeta \right\} dB, \quad (11) \\ &= \int_0^{B_m} \left\{ \int_{\zeta}^{B_m} f_{||}(\zeta, B - \zeta, \theta_B) dB \right\} d\zeta \end{aligned}$$

where the integral domain is shown in Fig. 2(a). From (7) and (11), $H_{m\perp}$ is given as

$$H_{m\perp}(B_m, \theta_B) = \int_0^{B_m} \frac{1}{B_m} \frac{\partial}{\partial \theta_B} \left\{ \int_{\zeta}^{B_m} f_{||}(\zeta, B - \zeta, \theta_B) dB \right\} d\zeta. \quad (12)$$

From a comparison of (10) with (12), f_{\perp} is estimated as

$$f_{\perp}(\zeta, B_m - \zeta, \theta_B) = \frac{1}{B_m} \frac{\partial}{\partial \theta_B} \left\{ \int_{\zeta}^{B_m} f_{||}(\zeta, B - \zeta, \theta_B) dB \right\}. \quad (13)$$

Equation (13) is rewritten as

$$f_{\perp}(\zeta, B, \theta_B) = \frac{1}{B + \zeta} \frac{\partial}{\partial \theta_B} \left\{ \int_0^B f_{||}(\zeta, B, \theta_B) dB \right\}. \quad (14)$$

C. Derivation from anhysteretic curve

The anhysteretic curve is obtained by applying the decaying alternating magnetic flux with biased direct magnetic flux density B_b . The resultant $\mathbf{p}_{\zeta}(B_b \mathbf{e}_{B||})$ is given by

$$\mathbf{p}_{\zeta}(B_b \mathbf{e}_{B||}) = B_b \mathbf{e}_{B||}. \quad (15)$$

Consequently, $\mathbf{H}_b(B_b \mathbf{e}_{B||}) = (H_{b||}, H_{b\perp})$ is written as:

$$H_{b||}(B_b, \theta_B) = \int_0^{B_b} f_{||}(\zeta, B_b, \theta_B) d\zeta \quad (16)$$

$$H_{b\perp}(B_b, \theta_B) = \int_0^{B_b} f_{\perp}(\zeta, B_b, \theta_B) d\zeta. \quad (17)$$

From (6) and (16), F is written as

$$\begin{aligned} F(B_b, \theta_B) &= \int_0^{B_m} H_{b\parallel}(B, \theta_B) dB \\ &= \int_0^{B_b} \left\{ \int_0^{B_s} f_{\parallel}(\zeta, B, \theta_B) d\zeta \right\} dB; \\ &= \int_0^{B_s} \left\{ \int_0^{B_b} f_{\parallel}(\zeta, B, \theta_B) dB \right\} d\zeta \end{aligned} \quad (18)$$

the domain of integration is shown in Fig. 2(b). From (7) and (18), $H_{b\perp}$ is given as

$$H_{b\perp}(B_b, \theta_B) = \int_0^{B_s} \frac{1}{B_b} \frac{\partial}{\partial \theta_B} \left\{ \int_0^{B_b} f_{\parallel}(\zeta, B, \theta_B) dB \right\} d\zeta. \quad (19)$$

By comparing (17) with (19), f_{\perp} is estimated from

$$f_{\perp}(\zeta, B, \theta_B) = \frac{1}{B} \frac{\partial}{\partial \theta_B} \left\{ \int_0^B f_{\parallel}(\zeta, B, \theta_B) dB \right\}. \quad (20)$$

IV. SIMULATION RESULTS

We now compare simulation results of the anisotropic vector models with the measured static magnetic property for the non-oriented silicon steel sheet JIS: 35A230 under the alternating and rotational magnetic flux condition.

A. Alternating magnetic flux condition

Fig. 3 shows simulated $B-H_{\perp}$ loops using the shape function (4) for alternating flux with $\theta_B = \pi/6$, where f_{\perp} in (4) is identified from the measured H_{\perp} . The shape function (5) is equivalent to (4) for the alternating input because $\theta_p = \theta_B$. Fig. 4 shows simulated $B-H_{\perp}$ loops with $\theta_B = \pi/6$ and $\pi/3$ using f_{\perp} determined from (14) and (20) without using the measured $B-H_{\perp}$ loops.

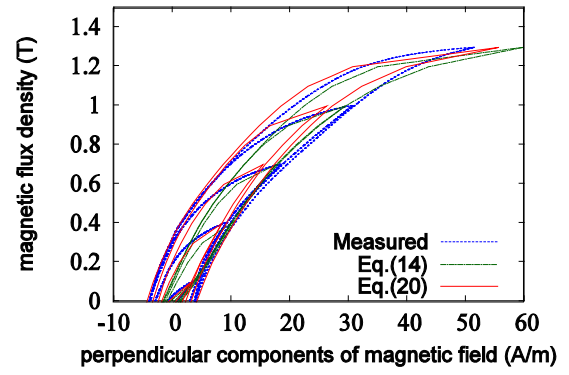
The proposed vector model using (4) represents $B-H_{\perp}$ loops more accurately than the simple model using (3). The shape function f_{\perp} identified from the measured H_{\perp} gives very accurate $B-H_{\perp}$ loops. The shape function f_{\perp} determined from (20) obtains more accurate $B-H_{\perp}$ loops than f_{\perp} determined from (14). Fig. 4 implies that the 2-D anisotropic vector hysteretic property can be reconstructed from the $B-H$ loops measured with the 1-D SST using the proposed anisotropic vector play model and the magnetic energy approach.

Fig. 5 shows the simulated iron loss per cycle for the alternating input with $\theta_B = 0, \pi/6, \pi/4, \pi/3$. This simulated loss agrees with the measured loss.

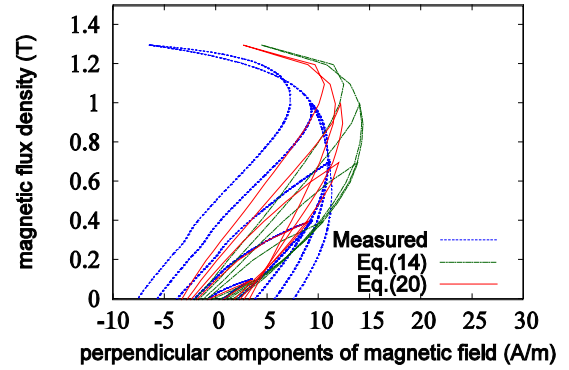
B. Rotating magnetic flux condition

Figs. 6 and 7 portray the simulated loci of \mathbf{H} for the clockwise (CW) rotational input of \mathbf{B} where the amplitude $B_a = 0.7, 1.0, 1.2, 1.3, 1.4$ T; the vector shape functions (4) and (5) are used with the shape function f_{\perp} determined from (20). The loci of \mathbf{H} for rotational inputs of \mathbf{B} are reconstructed from the $B-H$ loops measured with the 1-D SST. The vector shape function (5) is more accurate than (4) when the amplitude of \mathbf{B} is small.

If the measured rotational hysteresis loss is available, it is possible to adjust the simulated rotational hysteresis loss to the measured value by decomposing the vector shape function (5),



(a) $\theta_B = \pi/6$ [rad]



(b) $\theta_B = \pi/3$ [rad]

Fig. 4. Simulated $B-H_{\perp}$ loops using the shape function f_{\perp} determined from magnetic energy using (14) and (20).

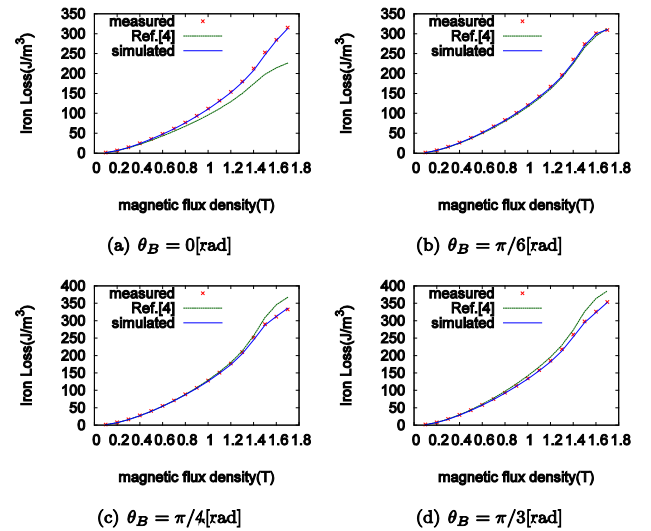


Fig. 5. Alternating hysteresis loss

$$\begin{aligned} f(\zeta, p_{\zeta}(\mathbf{B}), \theta_p) &= f_{\parallel\parallel} + f_{\parallel\perp} + f_{\perp\parallel} + f_{\perp\perp} \\ f_{\parallel\parallel} &= \left\{ f_{\parallel}(\zeta, |p_{\zeta}(\mathbf{B})|, \theta_p) \mathbf{e}_{p_{\parallel}} \cdot \mathbf{e}_{B_{\parallel}} \right\} \mathbf{e}_{B_{\parallel}} \\ f_{\parallel\perp} &= \left\{ f_{\parallel}(\zeta, |p_{\zeta}(\mathbf{B})|, \theta_p) \mathbf{e}_{p_{\parallel}} \cdot \mathbf{e}_{B_{\perp}} \right\} \mathbf{e}_{B_{\perp}} \\ f_{\perp\parallel} &= \left\{ f_{\perp}(\zeta, |p_{\zeta}(\mathbf{B})|, \theta_p) \mathbf{e}_{p_{\perp}} \cdot \mathbf{e}_{B_{\parallel}} \right\} \mathbf{e}_{B_{\parallel}} \\ f_{\perp\perp} &= \left\{ f_{\perp}(\zeta, |p_{\zeta}(\mathbf{B})|, \theta_p) \mathbf{e}_{p_{\perp}} \cdot \mathbf{e}_{B_{\perp}} \right\} \mathbf{e}_{B_{\perp}} \end{aligned} \quad (21)$$

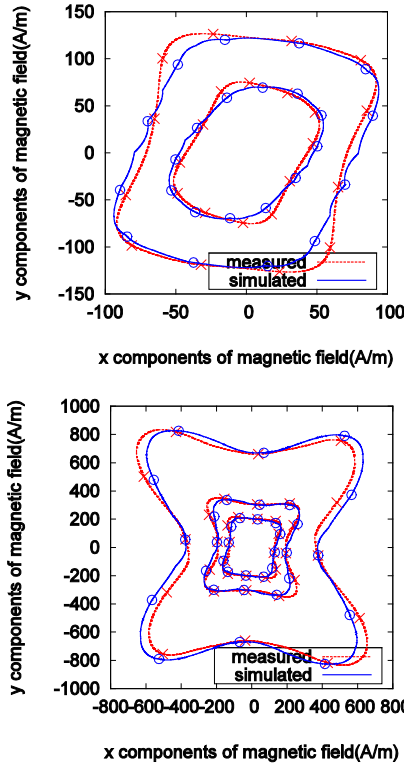


Fig. 6. Loci of H vector for rotational magnetic flux using (4).

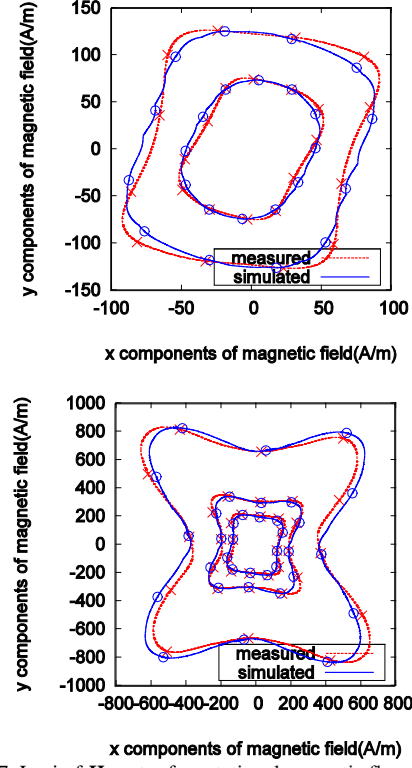


Fig. 7. Loci of H vector for rotational magnetic flux using (5).

where $e_{B\perp}$ is the unit vector perpendicular to B . The alternating property depends on $f_{\parallel\perp}$ and $f_{\perp\perp}$ whereas $f_{\parallel\perp}$ and $f_{\perp\parallel}$ do not appear for the alternating input because $e_{p\parallel} \cdot e_{B\perp} = e_{p\perp} \cdot e_{B\parallel} = 0$. The rotational hysteresis loss is affected by $f_{\parallel\perp}$ and $f_{\perp\perp}$. To adjust the rotational loss without affecting its alternating property, $f_{\parallel\perp}$ is modified to

$$f_{\parallel\perp}^* = \left(\frac{L_{\text{mea}} - L_{\perp\perp}(|B|)}{L_{\parallel\perp}(|B|)} \right) f_{\parallel\perp}, \quad (22)$$

where $L_{\perp\perp}$ and $L_{\parallel\perp}$ are simulated losses associated with $f_{\parallel\perp}$ and $f_{\perp\perp}$, and L_{mea} is the measured loss. This adjustment requires the measurement under the rotating magnetic flux condition using the 2D-SST, where the waveform control is relatively easy compared with the measurement under the alternating magnetic flux condition.

Fig. 8 shows the adjusted simulated iron loss per cycle of JIS:35A230 for the rotational input, which agrees with the measured loss.

V. CONCLUSION

The 2-D anisotropic vector hysteretic property can be reconstructed from the B - H loops measured with the 1-D SST, using the proposed anisotropic vector play model and the magnetic energy approach.

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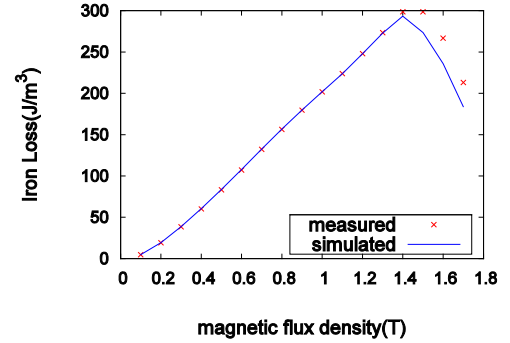


Fig. 8. Rotational hysteresis loss using (5).

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